

# Markov Chain Monte Carlo for Rare Event Reliability Analysis with Nonlinear Finite Elements

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Theory and Simulation of Failure Probabilities and Rare Events

David K. E. Green

School of Civil and Environmental Engineering  
University of New South Wales



**UNSW**  
AUSTRALIA

# Overview

**Question: Which MCMC methodology is most appropriate for Subset Simulation when sampling is computationally expensive?**

**Test case: a footing on soil with a nonlinear material model**

Contents:

- Briefly: Why rare event estimation is important in Civil Engineering
- Subset Simulation and Markov Chain Monte Carlo for FEM
- Numerical problem description
- Results and computational efficiency comparison

# Rare events: relevance and simulation challenges

## Risk in Civil Engineering:

Unacceptable performance carries severe consequences. Loss of life and large damage cost possible during failures. This necessitates that the probability of unacceptable performance is small.

## Rare event simulation for stochastic PDE based reliability analysis:

### Series expansion methods

- Faster than sampling for close to mean responses.
- Poor accuracy far from mean.
- Nonlinear material models are a challenge.

### Monte Carlo Simulation

- Fixed convergence rate ( $\frac{1}{\sqrt{N}}$ ) with number of simulations,  $N$ .
- Slow for far from mean response.
- Nonlinear material models only as challenging in the deterministic case.

# Subset Simulation

Denote the threshold event of interest as  $T$ .

Decompose the probability of  $T$  occurring as a series of conditional probabilities:

$$\mathbb{P}(T) = \mathbb{P}(T_1) \prod_i^{m-1} \mathbb{P}(T_{i+1}|T_i)$$

where:

$$T_1 \subset T_2 \subset \dots \subset T_m = T$$

Estimate  $\mathbb{P}(T_{i+1}|T_i)$  by Markov Chain Monte Carlo.

If sampled value  $\notin T_i$ , reject the sample and revert to previous sample value.

# Markov Chain Monte Carlo for Subset Simulation

As in regular Monte Carlo, estimate probabilities by sample estimate. For  $N$  FEM simulations:

$$\mathbb{P}(T_{i+1}|T_i) = \frac{1}{N} \sum_{j=1}^N \Psi(u_j)$$

where  $u_j$  is solution to  $j$ -th FEM simulation and  $\Psi(u_j) = 1$  if  $u_j$  has  $T_{i+1}$  occur and  $\Psi(u_j) = 0$  otherwise.

Monte Carlo Simulation draws the next sample from the input distribution independently of the previous sample.

Markov Chain Monte Carlo finds next sample by applying a transition function to the current sample.

## Error estimation - stationary Markov Chains

Central Limit Theorem for MCS and stationary Markov Chains:

$$\mathcal{N}\left(\mu, \frac{\sigma^2}{N}\right)$$

For stationary Markov Chains - MCMC mean estimate variance:

$$\sigma^2 = \text{Var}[\Psi(u)] + 2 \sum_{k=1}^{\infty} \text{Cov}[\Psi(u_j), \Psi(u_{j+k})]$$

Where  $\Psi(u_j)$  indicates  $u_j \in T_{i+1}$ . Let  $\Psi(u)$  represent  $\Psi(u_j)$  for all  $j$ .

Subset Simulation product probability distribution:

$$f_Z(z) = \int_{-\infty}^{\infty} f_Y\left(\frac{z}{x}\right) f_X(x) \frac{1}{|x|} dx$$

Can use this equation to numerically estimate confidence intervals.

# MCMC Sampling methodology summary

Metropolis-Hastings Ratio - Probability to update random walk sample

Acceptance ratio:  $\alpha = \frac{\mathbb{P}(\text{new})}{\mathbb{P}(\text{old})}$ . Accept new sample with probability  $\alpha$ .

Represent input sample as vector in  $\mathbb{R}^D$

Metropolis-Hastings (MH)	Gibbs Sampling	Componentwise- Metropolis-Hastings (CMH)
<ul style="list-style-type: none"> <li>• Update entire vector</li> <li>• Use transition function at previous result</li> <li>• Accept new value according to ratio</li> </ul>	<ul style="list-style-type: none"> <li>• Update single component</li> <li>• Update according to marginal distribution</li> <li>• Always accept new value</li> </ul>	<ul style="list-style-type: none"> <li>• Update single component</li> <li>• Use transition function at previous result</li> <li>• Accept new value according to ratio</li> </ul>

# MCMC Sampler efficiency for FEM analysis

The Subset Simulation MCMC sampler efficiency will depend on:

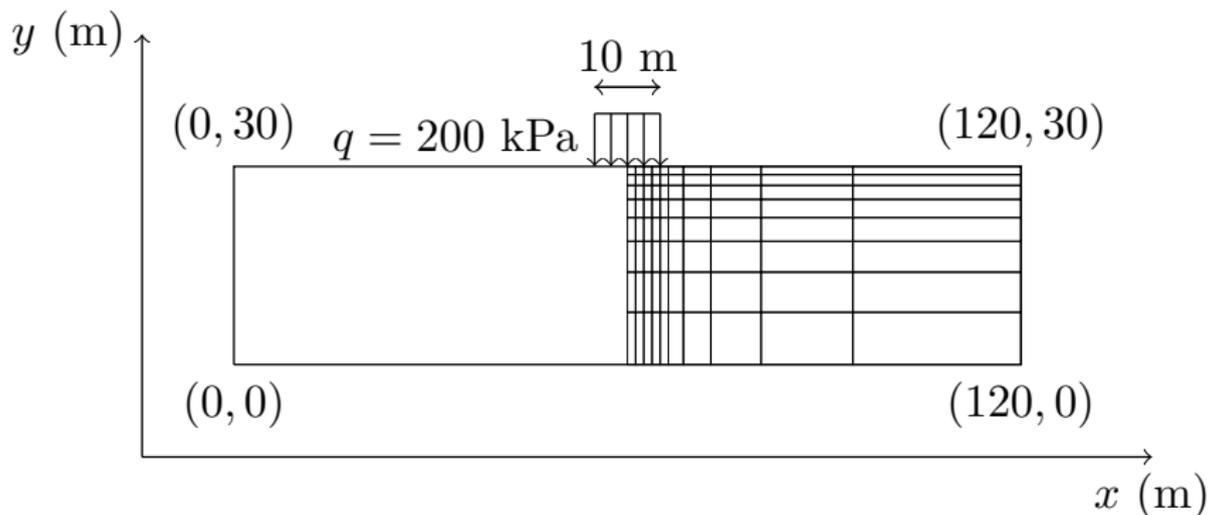
- **Minimising number of FEM analyses.** These are very computationally expensive. For nonlinear FEM, the difference is more pronounced than in linear FEM.
- **Ability to find new test locations quickly,** i.e. transition probabilities not too small.
- **Minimising the number of analyses conducted that do not meet the minimum threshold level.** Don't want to jump too far from current best location. A potential problem for Gibbs sampling, most likely to jump closer to the mean response rather than further away.

## Expected behaviour during analysis

### Will higher acceptance probability for Gibbs and CMH offset the potentially faster mixing of MH?

- MCS should become less efficient for small probabilities as the convergence rate is fixed
- Componentwise MCMC samplers should mix more slowly - more simulations required to explore sample space
- For computationally expensive sampling (i.e. nonlinear FEM), minimising the number of analyses is the time critical part of analysis
- MH sampler acceptance probability tends to zero for infinite probabilistic vector size. This may reduce simulation efficiency compared to Gibbs and CMH.
- On the other hand, failure to jump to a new location has little computational overhead, FEM equations do not have to be re-evaluated.

# Common problem geometry and parameters



Mesh - 80 elements.

Mean(E) = 50 MPa, CoV(E) = 0.2,  $\nu = 0.2$ .

Originally from: Sudret & Der Kiureghian (2002)

doi:10.1016/s0266-8920(02)00031-0

# Linear and nonlinear analysis

## Reliability analysis problem

Find  $\mathbb{P}(u > u_0)$ .  $u$  = vertical displacement at centre of footing.

- Two Subset Simulation tests - linear and nonlinear FEM problem
- Linear problem from: Sudret & Der Kiureghian (2002)  
doi:10.1016/s0266-8920(02)00031-0
- SSFEM results indicate  $\mathbb{P}(u > u_0^i) \approx 10^{-1}\mathbb{P}(u > u_0^{i-1})$
- Nonlinear problem presented adds more complex constitutive model

## Limit state values, $u_0$

$$u_0^1 = 60 \text{ mm}$$

$$u_0^2 = 80 \text{ mm}$$

$$u_0^3 = 100 \text{ mm}$$

$$u_0^4 = 120 \text{ mm}$$

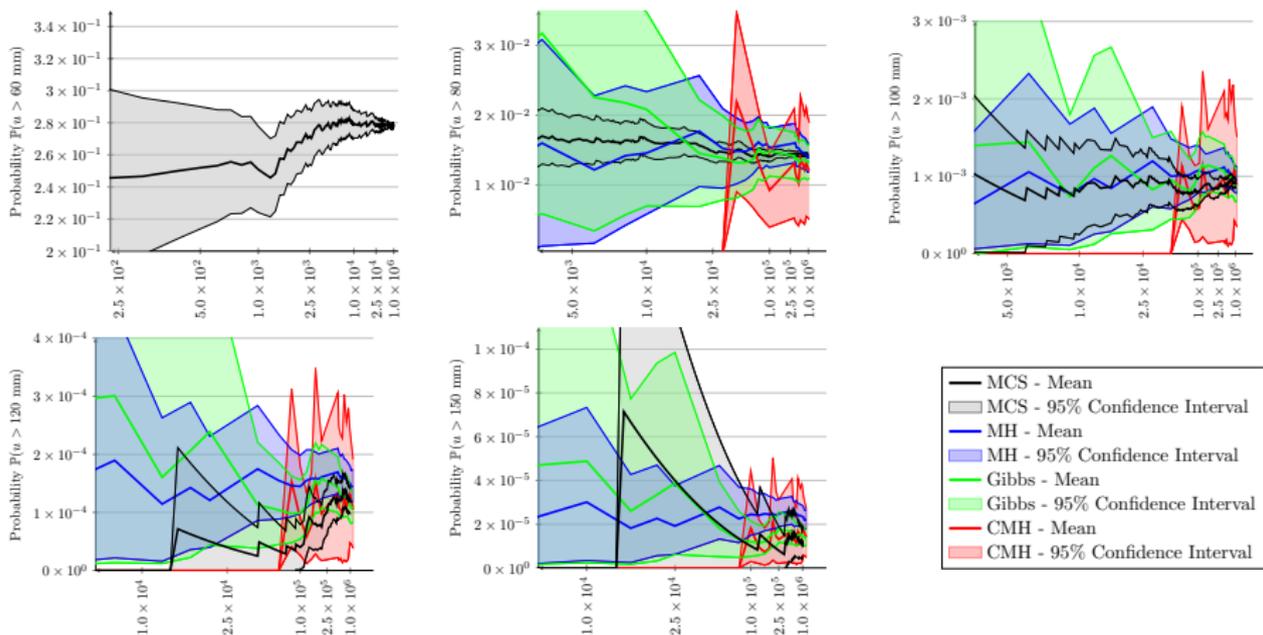
$$u_0^5 = 150 \text{ mm}$$

## Linear elastic problem

To test performance and convergence, a large number of simulations were carried out.

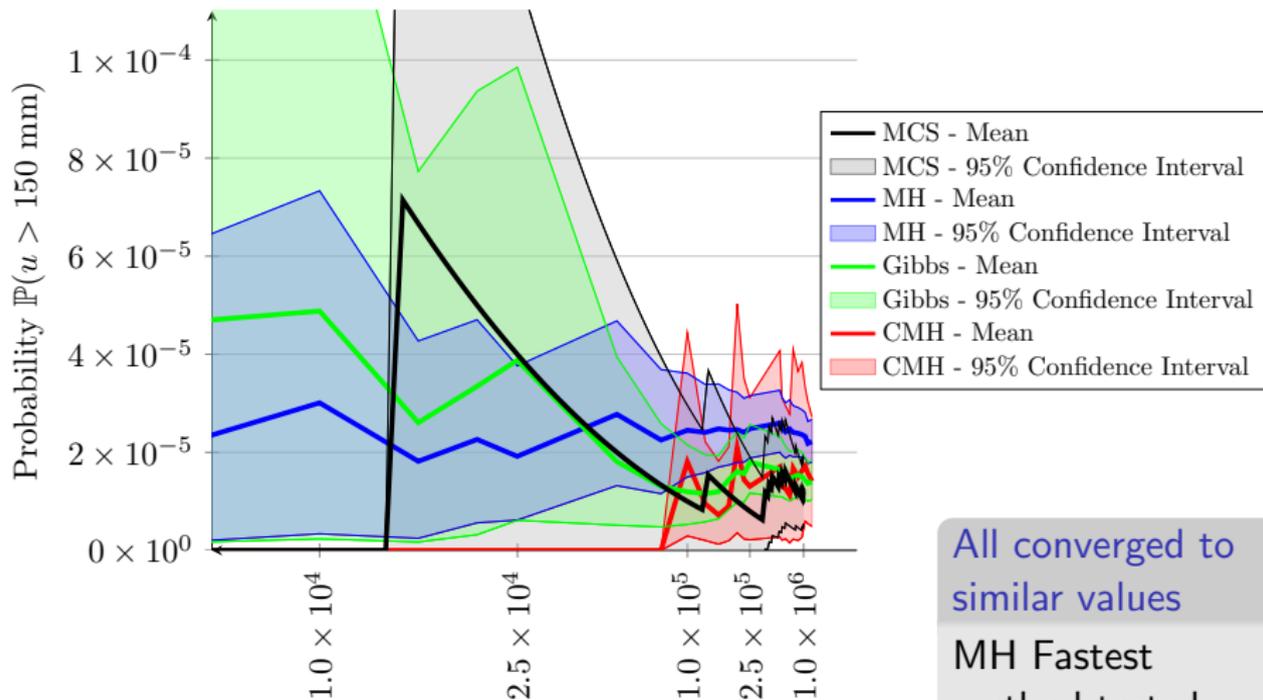
- E random field,  $\theta_x = \infty, \theta_y = 30$  m. Normally distributed, exponential decay correlation function.
- MCS, SSFEM and Subset Simulation convergence results compared.
- Subset Simulation - MH, Gibbs and CMH tested.
- MCS -  $1 \times 10^6$  simulations.
- Subset Simulation -  $1 \times 10^5$  per level. Number of simulations calculated cumulatively.
- For sampling methodologies: each linear analysis takes same amount of time to solve on average. Number of runs is reasonable for time comparison.

# Convergence vs number FEM simulations



X-axis all plots: Number of simulations,  $N$ . Scale =  $\frac{1}{\sqrt{N}}$

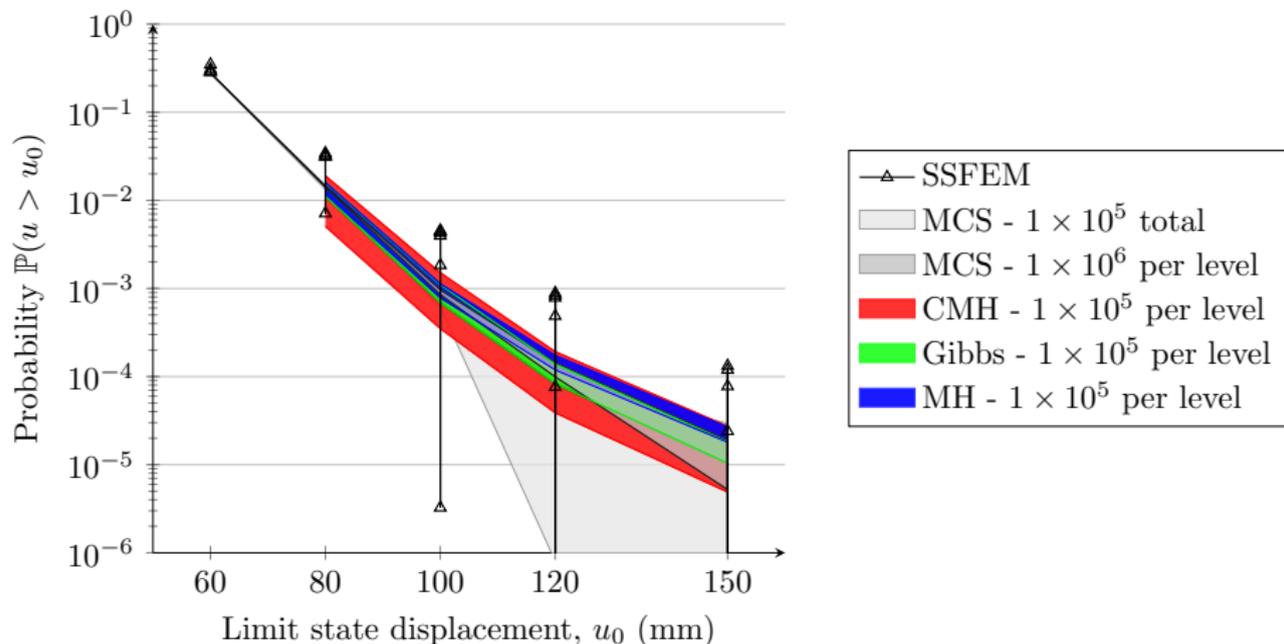
# Convergence vs FEM simulations - $\mathbb{P}(u > u_0 = 150 \text{ mm})$



All converged to  
similar values

MH Fastest  
method tested

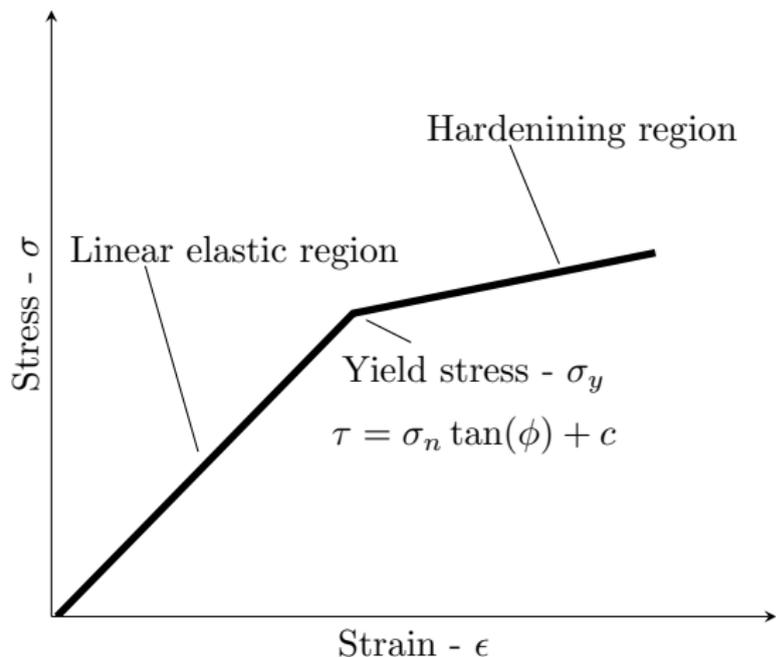
# Summary results - linear elastic parameters



# Elastic Problem - Discussion

- SSFEM, MCS and Subset Simulation in reasonable agreement. All techniques converged to similar values.
- MCS convergence improved with number of runs as expected.  $1 \times 10^6$  FEM simulations required to estimate  $\mathbb{P}(u > 150 \text{ mm})$  reasonably well.
- Subset Simulation much better than MCS for  $u_0 = 120$  and  $150 \text{ mm}$ .
- MH best convergence performance, followed closely by Gibbs.
- Oscillations in CMH mean prevented confidence interval convergence.
- Confidence interval estimation technique effectively captures range of possible values.

# Nonlinear FEM problem - constitutive model



For the nonlinear analysis, a Mohr-Coulomb constitutive model was introduced.

$E$ ,  $\phi$  and  $c$  - random fields (Normally distributed).

All correlation lengths set to  $\theta_x = 10$  m,  $\theta_y = 30$  m.

Very small hardening parameter,  $\psi$ , included.

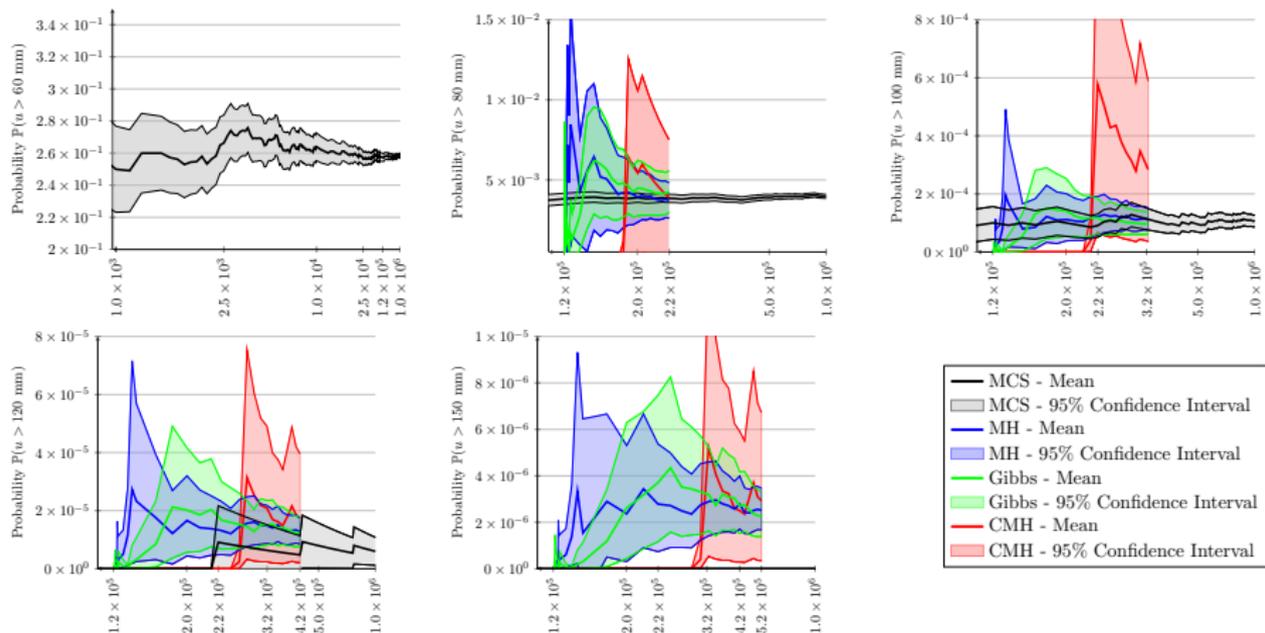
## Nonlinear FEM - problem description

To match a more realistic analysis, the following analyses were carried out:

- For  $\mathbb{P}(u > u_0 = 60 \text{ mm})$ , MCS run until 1% relative error.
- For all other Subset Levels,  $1 \times 10^5$  MCMC simulations carried out.
- MH, CMH and Gibbs sampling tested.
- To verify, the MCMC analysis  $1 \times 10^6$  MCS simulations were run.

**The convergence rate and efficiency of each method was compared.**

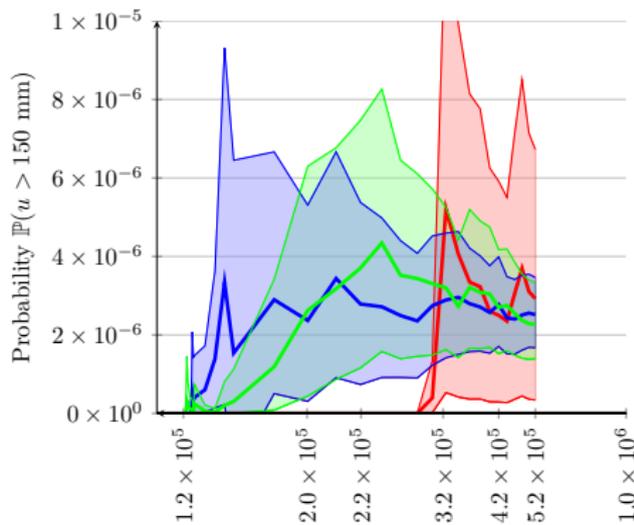
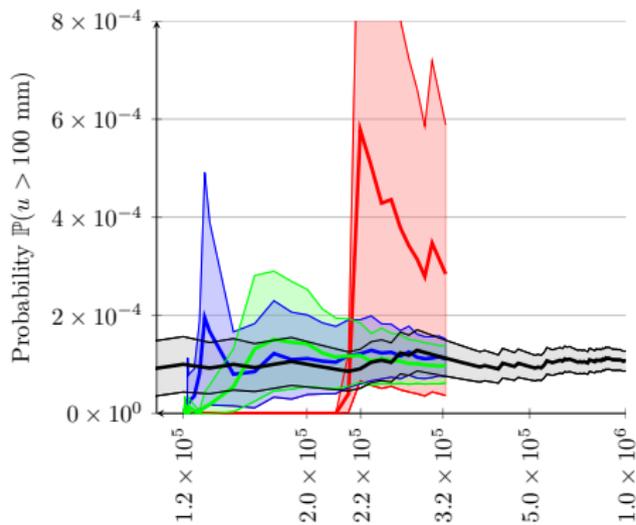
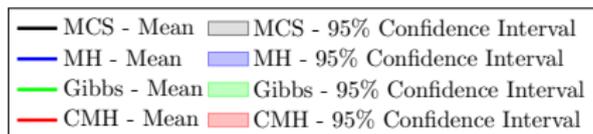
# Convergence vs number FEM simulations



X-axis all plots: Number of simulations,  $N$ . Scale =  $\frac{1}{\sqrt{N}}$

MCS relative error of 1% found after approximately  $1.2 \times 10^5$  simulations.

# CMH - poor estimate for $u_0 = 100$ mm recovery

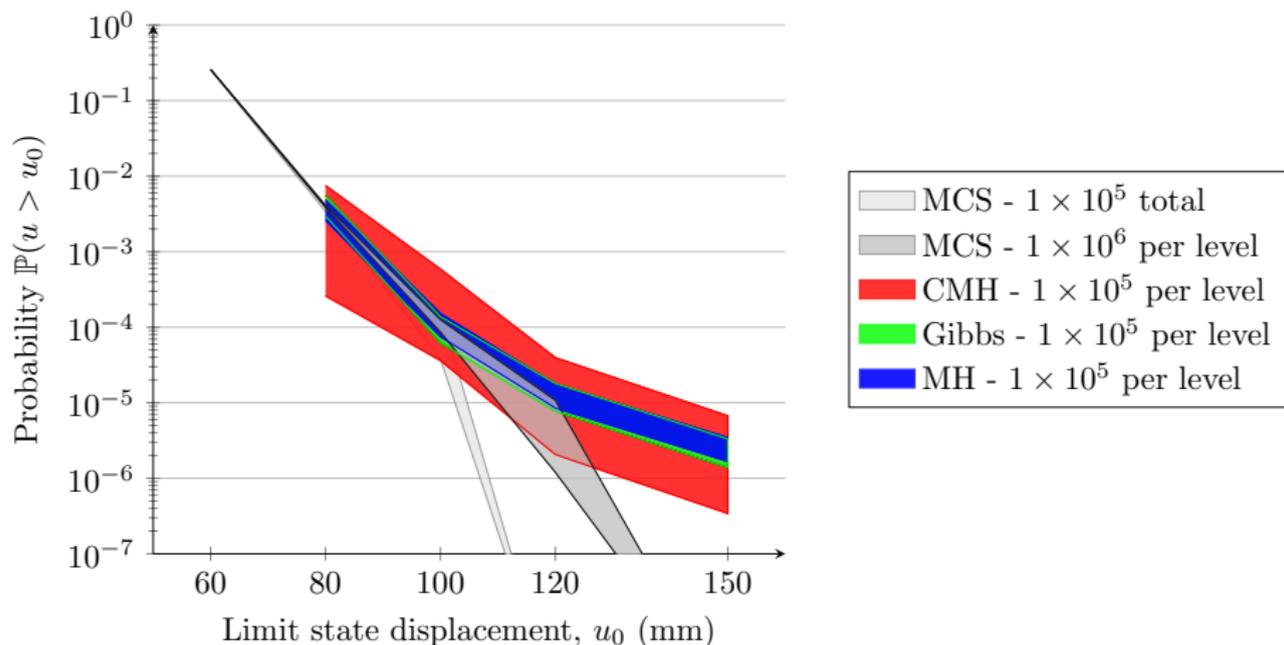


X-axis all plots: Number of simulations,  $N$ . Scale =  $\frac{1}{\sqrt{N}}$

# Nonlinear analysis - trace plots

- As in the elastic case, all values converged to similar estimates.
- For  $u_0 = 120$  and  $150$  mm:
  - $\mathbb{P}(u > 120 \text{ mm}) \approx 10^{-5}$
  - $\mathbb{P}(u > 150 \text{ mm}) \approx 10^{-6}$
- MCS would require millions of runs for accurate estimates for  $\mathbb{P}(u > 150 \text{ mm})$  and  $u_0 > 150$  mm.
- CMH, again, displayed slower mixing than other MCMC methods. Long period spent below threshold, long period spent above threshold.
- Subset Simulation able to recover from earlier poor estimates.
- Confidence intervals critical for understanding mean estimates.

# Summary results - nonlinear parameters



# Nonlinear analysis - efficiency estimates

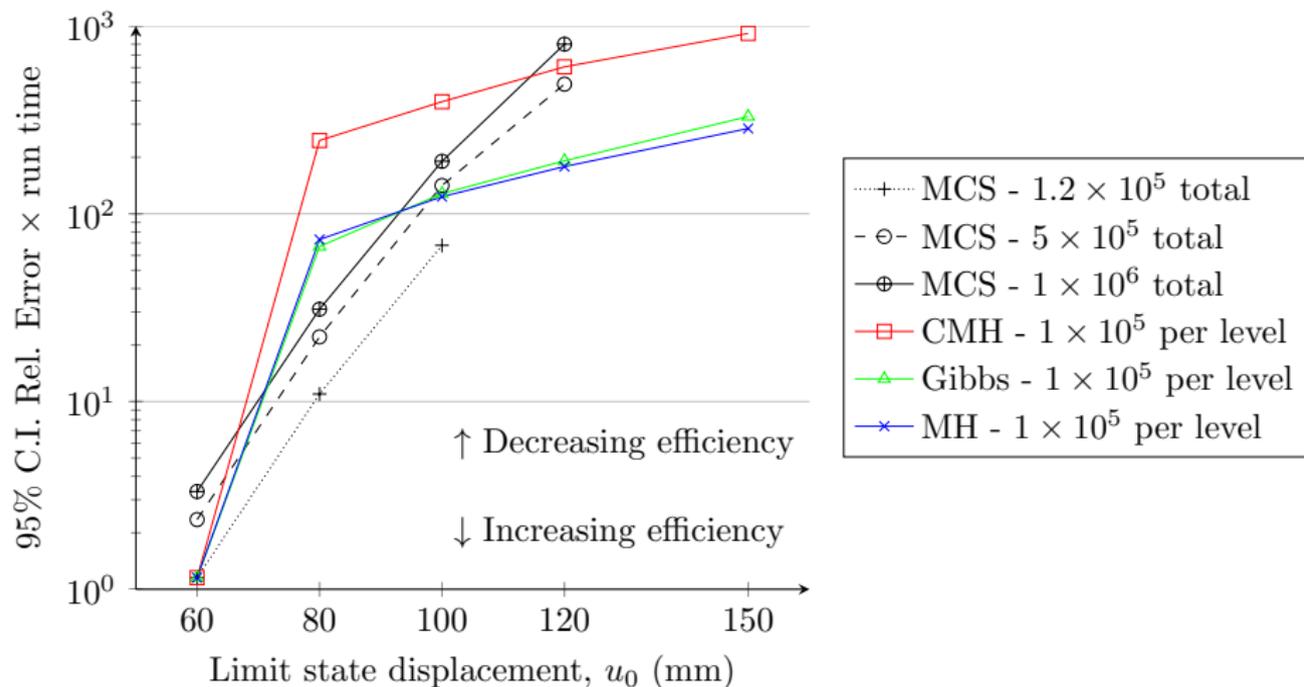
## Simulation technique efficiency compared by:

### Relative computational cost estimate

$$\text{Computational Cost} = (\text{Run time}) \times (95\% \text{ C.I. Rel. Err.})$$

- Time normalised by setting time for  $1 \times 10^5$  by MCS simulations to 1 unit
- Relative error taken as average 95% confidence interval width.
- As all Subset Simulation analyses used the same  $\mathbb{P}(u > 60 \text{ mm})$ , the MCMC efficiency could be compared.

# Nonlinear analysis - efficiency



# Nonlinear analysis - efficiency

## Monte Carlo Simulation:

- More efficient closer to mean.
- By  $u_0 = 100$  mm, efficiency becomes worse than Subset Simulation.

## Subset Simulation - all methods started using same $\mathbb{P}(u > 60 \text{ mm})$ :

- CMH slow mixing degrades efficiency by preventing confidence interval convergence.
- Gibbs and MH very similar performance.
- Further from mean response, MH begins to outperform Gibbs.
- Analyses suggest that for further from mean responses, MH had best performance.

# Nonlinear analysis - conclusions

## Sampling efficiency observations and explanations:

- Subset Simulation is more efficient than direct MCS far from the mean.
- Componentwise sampling reduces simulation efficiency.
- Gibbs sampling - away from the mean, sampling from the full marginal makes it more likely to sample below the minimum Subset level threshold (than MH or CMH).
- In contrast, MH sampling doesn't jump far enough to fall below the minimum threshold level as often.
- For computationally expensive sampling, it is better to take more time to find a good sample (by MH) than to take many poor samples (CMH and Gibbs).

## High dimensional acceptance probability problem in MH?

If acceptance probability becomes too small, update maximal batches of probabilistic vector per iteration.

# Conclusions

- For analyses conducted, Subset Simulation was effective for estimating rare event, far from mean responses.
- Metropolis-Hastings was best performing MCMC sampler.
- Gibbs performance similar, but degraded further from mean.
- Componentwise Metropolis-Hastings displayed oscillatory behaviour around estimated value.
- Confidence interval estimator worked well to capture range of variations.

# Thank you!